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# Ca-Cu/Al $_2$ O $_3$ catalysts for H $_2$ S removal at near ambient temperature: Synthesis, characterization, DFT calculation, and mechanistic insights

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#### ABSTRACT

A series of Ca-doped  $Cu_xO/Al_2O_3$  catalysts were developed using the excessive impregnation method for  $H_2S$  catalytic oxidation at near-ambient temperatures.  $Ca(NO_3)$ - $Cu_xO/Al_2O_3$  catalyst with 2.5 wt% Ca exhibited optimal  $H_2S$  desulfurization performance at 60 °C and RH 60%, achieving an  $H_2S$  removal capacity of 401.34 mg/g. Experimental, characterization, and DFT calculation results demonstrate that during the catalytic oxidation of  $H_2S$ ,  $H_2O$  can be catalytically convert into ·OH while simultaneously capturing and dissociating  $H_2S$ . The ·OH and  $NO_3$  then catalyze the oxidation of  $H_2S$  to elemental S. Moreover, the redundant OH adsorbed on the basic sites can buffer the pH and promote the dissociation of  $H_2S$ . The above cyclic process could alleviate the deactivation of the Ca- $Cu/Al_2O_3$  catalyst. Therefore, a ·OH-induced desulfurization mechanism assisted with  $Ca^{2+}$  buffer the pH and  $NO_3$  cyclic oxidation of  $H_2S$  has been proposed. This work contributes to the preparation of high-capacity mental-based catalysts for  $H_2S$  oxidation.

#### 1. Introduction

As a colorless, corrosive, and highly toxic gas with a distinctive odor reminiscent of rotten eggs, hydrogen sulfide ( $H_2S$ ) is prevalent in numerous chemical processes, landfills, and shale gas formations, permeating diverse environments. [1,2].  $H_2S$  has the potential to corrode transportation pipelines and buildings, contribute to the formation of acid rain in the atmosphere, degrade the environment, and pose health risks to humans [3,4]. With a remarkably low olfactory threshold of 0.0008  $mg/m^3$ , even at low concentrations,  $H_2S$  can cause discomfort. Therefore, reducing  $H_2S$  emission levels below the olfactory threshold is crucial to minimize its influence on the environment and human health [5].

Under appropriate conditions, selective catalytic oxidation (SCO) offers a highly effective means of completely converting  $\rm H_2S$  into sulfur.

This makes it particularly suitable for the efficient and thorough removal of  $H_2S$ , thereby establishing SCO as a hot topic [1,6,7]. SCO technology can be categorized into two classes, taking into account the reaction temperature about the sulfur dew point (approximately 180 °C): high-temperature (> 180 °C)  $H_2S$ -SCO technology and low-temperature (< 180 °C)  $H_2S$ -SCO technology. The high-temperature  $H_2S$ -SCO technology, primarily based on the Claus process, can achieve desulfurization efficiencies of only 99.2–99.5%, even under the most stringent conditions [7-9]. The sulfur converted from  $H_2S$  can also oxidize into SO<sub>2</sub>, causing secondary pollution [7]. Therefore, the high-temperature  $H_2S$ -SCO technology is unsuitable for locations that do not meet the thermodynamic requirements and residential areas with strict  $H_2S$  treatment regulations. In the low-temperature  $H_2S$ -SCO process, sulfur condenses and is stored within the catalyst's pore structure, achieving a 100% removal rate of  $H_2S$  [7,10,11]. This technology is

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suitable for situations with no thermodynamic conditions and strict requirements for  $H_2S$  treatment. The core of this technology lies in the catalyst used.

Metal oxides are the main active phases for H2S desulfurization, such as the oxides of Ag, Cu, Zn, Co, Ni, Ca, Mg, V, and Sn [12-16]. Among the various metal oxides, copper is widely employed in catalysis owing to its high activity and cost-effectiveness. In particular, CuO demonstrates exceptional catalytic performance for H<sub>2</sub>S and finds widespread use in low-temperature H<sub>2</sub>S-SCO processes. Due to its large particle size, inadequate specific surface area (SSA), and limited micro- and meso-pores, the single-metal oxide (MO) exhibits a low H2S removal efficiency. Researchers have developed a solution to overcome these challenges by dispersing MOs onto highly porous supports, thereby reducing particle size [13,17-22]. This approach increases the SSA, improves metal stability, and enhances the H<sub>2</sub>S removal. Supporting Cu<sub>x</sub>O on γ-Al<sub>2</sub>O<sub>3</sub> is reported to significantly enhance its H<sub>2</sub>S desulfurization performance [23]. This is attributed to the large SSA, pore volume, and hydrophilicity of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, which significantly improve the H<sub>2</sub>S desulfurization performance of Cu<sub>v</sub>O. Furthermore, the H<sub>2</sub>S desulfurization performance is further enhanced by doping a second component

It has been reported that the desulfurization performance of a catalyst can be improved by its surface basicity or the presence of basicity groups. Introducing a basic metal into the catalyst is an effective method to increase its surface basicity. Commonly used alkaline impregnating solutions include Na<sub>2</sub>CO<sub>3</sub>, NaOH, K<sub>2</sub>CO<sub>3</sub>, KOH, and Mg(NO<sub>3</sub>)<sub>2</sub> [25-27]. Researchers have discovered that alkaline earth Mg performed better performance than conventional alkaline salts [25]. Calcium (Ca), also an alkaline earth metal, is widely used as a desulfurizing agent for hot flue gas SO<sub>2</sub> removal due to its lower cost and environmental friendliness [28]. Recently, excellent desulfurization performance has been achieved by supporting CaO on activated carbon in the low-temperature H<sub>2</sub>S-SCO process [29]. Moreover, it has been found that the low reactivity adsorption of H2S by Ca prevents its conversion into sulfides, thus slowing down catalyst deactivation [24]. Additionally, the high alkalinity of Ca facilitates the dissociation of H<sub>2</sub>S [30]. Therefore, it is reasonable to enhance the desulfurization performance of Cu<sub>x</sub>O/γ-Al<sub>2</sub>O<sub>3</sub> by utilizing the high alkalinity of Ca, especially by exploiting the oxidizing property of NO<sub>3</sub> in alkali metal nitrates. By combining the advantages of Cu<sub>x</sub>O/γ-Al<sub>2</sub>O<sub>3</sub> with the prominent characteristics of Ca<sup>2+</sup> and NO<sub>3</sub>, it is expected to develop an ideal catalyst. Previous studies have mainly focused on using single or multiple metal oxides as active components for H<sub>2</sub>S removal [3,10,15,17,18,20-24]. The simultaneous utilization of nitrates and metal oxides as active components for low-temperature H2S removal was rarely reported. Moreover, the understanding of the reaction mechanism is still unknown, which hampers the rational application and optimization of metal-based catalysts.

In this study, the objective was to develop efficient and stable catalysts for the low-temperature  $\rm H_2S$ -SCO process. To achieve this, a group of  $\rm Ca(NO_3)_2\text{-}Cu_xO/Al_2O_3$  catalysts with different loadings of Ca were prepared. The performance of these catalysts in  $\rm H_2S$  removal was examined under various humidity and temperature. The catalysts were comprehensively characterized before and after  $\rm H_2S$  removal, and DFT calculations were employed to propose potential desulfurization mechanisms. This catalyst shows promise as an effective solution for low-temperature  $\rm H_2S$  removal.

#### 2. Experimental

#### 2.1. Materials

Activated alumina ( $\gamma$ -Al $_2$ O $_3$ ), calcium nitrate hydrate (Ca (NO $_3$ ) $_2$ ·H $_2$ O) and copper nitrate hexahydrate (Cu(NO $_3$ ) $_2$ ·3 H $_2$ O), and were obtained from China National Medicines Co., LTD, all of which were analytical grade.

#### 2.2. Catalyst preparation

 $Al_2O_3$  supported with a Ca-Cu composite was synthesized using the excessive impregnation method. After determining the superior  $H_2S$  removal performance,  $Cu_xO/Al_2O_3$  (3 wt%) was chosen. The preparation procedure is described as follows: impregnate 5 g of  $\gamma\text{-}Al_2O_3$  particles with a size range of 380–830  $\mu m$  in 20 mL of  $Cu(NO_3)_2$  solution with a concentration of 0.776 mol/L, followed by 30 min of ultrasound treatment, and continue the immersion at rest for 11.5 h. The wet catalyst was then dried in an oven for 30 min at 60 °C. Subsequently, the catalysts were heated at a heating rate of 5 °C/min until reaching a temperature of 500 °C in a muffle furnace. Then it was calcinied for 4 h under atmospheric conditions at 500 °C.

To further study the influence of Ca-compound on the  $H_2S$  desulfurization performance,  $Ca/Al_2O_3$  samples were also synthesized. The preparation procedure for the  $Ca/Al_2O_3$  catalyst, which contained 2.5 wt%  $Ca^{2+}$ , was as follows: Initially, 5 g of  $\gamma$ - $Al_2O_3$  were immersed in a 20 mL solution containing 3.59 g of  $Ca(NO_3)_2 \cdot H_2O$ . The subsequent impregnation, drying, and calcination steps were identical to those used to prepare the  $Cu_xO/Al_2O_3$  catalyst.

The Ca content optimization was performed based on the previously prepared  $\rm Cu_xO/Al_2O_3$  catalyst (3 wt%). We utilized a sequential impregnation technique to prepared the Ca-Cu\_xO/Al\_2O\_3 catalysts. Ca (NO\_3)\_2·4 H\_2O weighing 0.51 g, 1.54 g, 2.56 g, 3.59 g, and 4.61 g was dissolved in 20 mL of distilled water to obtain a Ca(NO\_3)\_2 solution. The Ca(NO\_3)\_2 solution was then used to prepare Ca-Cu\_xO/Al\_2O\_3 catalysts with corresponding Ca/catalyst ratios of 1 wt%, 1.5 wt%, 2 wt%, 2.5 wt %, and 3 wt%, respectively. The subsequent steps of impregnation, drying, and calcination followed the same procedure as the preparation steps for Cu\_xO/Al\_2O\_3. Quantification of Ca was achieved through the use of inductively coupled plasma-optical emission spectrometry (ICP-OES, Optima5300DV).

#### 2.3. Performance tests

Dynamic  $H_2S$  removal tests were conducted using a fixed bed adsorber under atmospheric pressure conditions. Specifically, 1 g of catalyst was placed in an acrylic tube with an inner diameter of 14 mm. Prior to the test, the catalyst was prewetted for 30 min at a flow rate of 120 mL/min. The prewetted catalyst was then exposed to a mixed gas stream in a reactor, comprising moisture-containing air and  $H_2S/N_2$ , flowing at a total rate of 150 mL/min. The initial  $H_2S$  concentration in the system was measured at  $1390 \pm 76$  mg/m $^3$ . A mass flow controller (Sevenstar CS100) regulated the gas flow rate. The gas humidity (RH 0–80%) and reaction temperature (40–70 °C) were regulated separately using a steam generator and a temperature controller. The concentration of  $H_2S$  was determined using a Shimadzu GC2010 chromatograph equipped with a flame photometric detector (FPD). Fig. S1 illustrates the test device utilized. The data was recorded through at least three measurements, with an error range not exceeding 5% to ensure experiment repeatability.

The test was concluded when the  $H_2S$  concentration reached 76 mg/  $m^3$  at the outlet. The catalyst's performance was assessed by determining its breakthrough sulfur capacity (S $_{\!c}$ , mg  $H_2S/g$  catalyst). This capacity was calculated using the following equation:

$$S_c = \frac{M * u * \left( \int_0^t (c_{in} - c_{out}) dt \right)}{10^6 * V_{mol} * m}$$
 (1)

Where: M is the molecular mass of  $H_2S$  (34 g/mol), u is the flow rate of the the  $H_2S/N_2$  mixed gas (150 mL/min in this study),  $c_{in}$  and  $c_{out}$  are the  $H_2S$  concentrations at the inlet and outlet, respectively (1390 and 76 mg/m $^3$  respectively in this study), t is the time taken to reached 76 mg/m $^3$  (min).  $V_{mol}$  is the molar volume of gas (22.4 L/mol at standard conditions). m is the mass of the catalyst in the reactor (1 g in this study).

#### 2.4. Sulfur recovery experiment

The sulfur recovery experiment was conducted in a vertical tubular furnace (Fig. S2). The specific operating procedures and test devices are shown in the supplementary material.

#### 2.5. Characterization

To examine the pore structure, the N2 adsorption-desorption isotherms of the samples were measured at −195.8 °C using a TRISTAR II 3020 M instrument. The sample's surface area was determined using the standardized Brunauer-Emmett-Teller (BET) method, while the pore volume was calculated using the Barrett-Joyner-Halenda (BJH) method. Scanning electron microscope (SEM) and energy dispersive X-ray (EDX) images were obtained using a Hitachi SU-8010 instrument to examine the catalyst's surface morphology and element distribution. To analyze the crystal structure of the catalyst, X-ray diffraction (XRD) was performed using a SmartLab smart X-ray diffractometer, with diffraction angles tested in the range of 10-80°. X-ray photoelectron spectroscopy (XPS) was performed using a PHI Quantera SXM spectrometer to assess the chemical states of surface elements. The microstructure was examined using a JEOL JEM-F200 transmission electron microscope (TEM) apparatus from Japan. Fourier transform infrared (FTIR) spectra were acquired using an X70 combined thermal analysis system from Netzsch, Germany to investigate the presence of functional groups on the catalyst surface. The Netzsch STA2500 instrument was utilized to conduct thermogravimetric analysis-derivative thermogravimetry (TG-DTG) testing for detecting weight loss of the samples with increasing temperature. The catalysts' CO<sub>2</sub> temperature-programmed desorption (CO<sub>2</sub>-TPD) was performed on an AUTO CHEM 2920 instrument. The surface defect and hydroxyl radicals (·OH) analysis were examined using electron paramagnetic resonance (EPR) analysis conducted on a Bruker EMXPLUS spectrometer. To assess the catalysts' ability to generate ·OH, a DMPO aqueous suspension was utilized as the capturing agent.

#### 2.6. Computational method

The Vienna Ab-initio Simulation Package (VASP) was used to conduct Density Functional Theory (DFT) calculations utilizing the generalized gradient approximation (GGA) and applying the Perdew-Burke-Ernzerho (PBE) formulation [31,32]. To describe the valence electrons and elucidate the characteristics of the ionic nuclei, we employed the method of using projected augmented wave (PAW) potentials in combination with a basis set consisting of plane waves. A specific cutoff energy of 520 eV [33,34] was chosen for this purpose. To accommodate partial occupancies of the Kohn-Sham orbitals, we implemented the Gaussian smearing method with a smearing width of 0.05 eV. The self-consistency of the electronic energy was established when the energy variation fell below 10-5 eV. To attain convergence in the geometry optimization process, we set the threshold for force change at a value lower than 0.05 eV/Å. To account for dispersion interactions, Grimme's DFT-D3 methodology [35] was incorporated. Following this, a surface model was constructed, possessing periodicity in both the x and y directions, and an independent periodicity in the z direction. To isolate the surface slab from its periodic replicas, we introduced a vacuum layer with a thickness of 18 Å.

The equilibrium lattice constants of CuO, Cu<sub>2</sub>O, and Ca(NO<sub>3</sub>)<sub>2</sub> unit cells were optimized. These were then used to construct a CuO, Cu<sub>2</sub>O, Ca (NO<sub>3</sub>)<sub>2</sub> (110) surface model. In order to optimize the structure, a  $3\times3\times1$  k-point grid was utilized for k-point sampling within the Brillouin zone. The bottom two atomic layers remained fixed during this process, while the top two layers were allowed to relax. The Cu<sub>2</sub>O-CuO structures were established using the Cu<sub>2</sub>O surface and CuO surface with the lattice parameters (a=18.1566 Å, b=13.4678 Å, c=28.8571 Å). The Cu<sub>2</sub>O-CuO structures with 6 layers of Cu-O-Cu layers included 172 atoms. Similarly, in the context of structural optimizations, a k-point grid of  $3\times3\times1$  was

implemented to sample the Brillouin zone and ensure accuracy. In this process, the bottom two atomic layers were held fixed, while relaxation was permitted for the top two layers (Fig. S3). CuO-Cu<sub>2</sub>O-Ca(NO<sub>3</sub>)<sub>2</sub> structures were established using the Cu<sub>2</sub>O surface, CuO surface, and Ca (NO<sub>3</sub>)<sub>2</sub> surface with the lattice parameters (a=18.9361 Å, b=13.5183 Å, c=28.8571 Å) (Fig. S4).

During structural optimizations, we sampled the Brillouin zone at the  $\Gamma$  point for k-point sampling, enabling all atoms to relax. Using the equation (Eq. 2), the calculation was performed to determine the free energy of  $H_2S$  on the surface or that of an adsorbate:

$$G = E + ZPE - TS (2)$$

where ZPE is the zero-point energy, E represents the total energy, T is the temperature in Kelvin (in this case, set as  $333.15~\rm K$ ), and S represents the entropy.

#### 3. Result and discussion

#### 3.1. Characterization of Ca-doped Cu-based catalysts

To obtain the surface and pore properties of samples, the  $N_2$  adsorption—desorption experiment was performed (Fig. 1 and Table 1). The prepared catalysts were designated as  $Cat_{CaxCu3}$ , where x represents the mass fraction (%) of calcium, and the mass fraction (%) of copper defaults to  $3\pm0.1\%$ . As shown in Fig. 1, all the isotherms of the samples exhibited a type IV shape with a distinct H3 hysteresis loop. Such hysteresis loops are typically observed in materials with slit-shaped pores that have non-uniform size and/or shape [36]. Table 2

The pore widths of all samples are in the range of 3-11 nm, indicating that they all possess a typical mesoporous structure [37]. It can be observed that with the increase in metal content, the H3 hysteresis loop shifts towards higher P/P<sub>0</sub> values, indicating a narrower distribution range of pores. This suggests that the metal may preferentially occupy smaller pores during loading. The Ca/Al<sub>2</sub>O<sub>3</sub> sample has the largest SSA, with 2-3 nm smaller pore sizes than those of the Al<sub>2</sub>O<sub>3</sub> matrix, while the pores in other width ranges remain almost constant. The total pore volume (TPV) did not decrease, but the average pore width was reduced. This may be attributed to the growth of microporous nanosheets on the surface of the Ca/Al<sub>2</sub>O<sub>3</sub> sample. The SSA of the Cat<sub>Cu3</sub> decreased with the loading of Cu oxides, and further decreased with the loading of Ca-compounds due to the deposition of metal oxides in minute pores (2-3 nm). It can be found that the SSA of Cat<sub>Ca2.5Cu3</sub> exhibits a significant increase, which may be attributed to the formation of microporous nanosheets. However, the low SSA of Cat<sub>Ca3Cu3</sub> suggests that the formation of nanosheets requires a specific concentration. Furthermore, the largest TPV and pore width of Cat<sub>Ca2.5Cu3</sub> suggested that the nanosheets composed of CuO and Ca-compounds have more micropores and mesopores than those grown by Ca-compounds. This implies that there are more H2S adsorption and conversion sites and additional product storage space available, which is advantageous for H<sub>2</sub>S removal [38,39].

The related samples were studied by SEM to gain insights into the influence of Ca compounds on the morphology of catalysts. Representative micrographs of all samples are shown in Fig. S5. For comparison, images of  $Al_2O_3$  are also presented. A three-dimensional (3D) nano-sheet structure can be observed on the surface of  $Ca/Al_2O_3$ , which is the reason for its high SSA. In contrast, the  $Cu/Al_2O_3$  surface exhibits rough and uneven particles, but after adding Ca, irregular small particles of various sizes appear on the catalyst surface. As the content of Cacompounds on the surface increases, these particles gradually accumulate. When the Ca content reaches 2.5 wt%, the catalyst displays a layered structure with nano-sheets (Fig. S6). However, with further increases in Ca compound content, these particles gradually agglomerate into larger clusters and the nano-sheet structure disappears. The SEM morphology change of the catalyst explains the reason for the increase and then decrease in SSA with increasing Ca content. Additionally, the

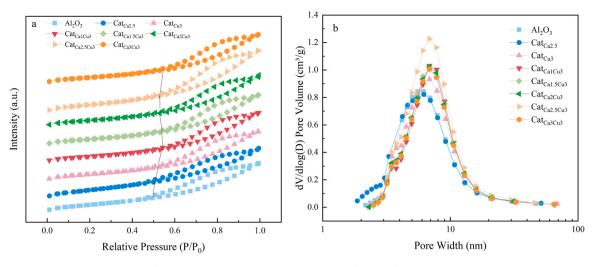


Fig. 1. The  $N_2$  adsorption-desorption isotherms (a) and pore width (b) of  $Cat_{CaxCu3}$ .

**Table 1**The properties of all Cat<sub>CaxCu3</sub>.

Sample	Metal content (wt%)		SSA (m <sup>2</sup> /g)	TPV (cm <sup>3</sup> /g)	Average Pore width (nm)
	Ca	Cu			
Al <sub>2</sub> O <sub>3</sub>	0	0	231	0.45	6.1
CaO/Ca (NO <sub>3</sub> ) <sub>2</sub>	/	/	18	0.03	/
CuO	/	/	15	0.04	/
Cat <sub>Ca2.5</sub>	2.5	0	267	0.45	5.8
Cat <sub>Cu3</sub>	0	3	204	0.45	6.6
Cat <sub>Ca1Cu3</sub>	1	3	196	0.45	6.9
Cat <sub>Ca1.5Cu3</sub>	1.5	3	191	0.45	7.0
Cat <sub>Ca2Cu3</sub>	2	3	198	0.44	6.7
Cat <sub>Ca2.5Cu3</sub>	2.5	3	245	0.56	6.8
Cat <sub>Ca3Cu3</sub>	3	3	193	0.44	6.8
Cat <sub>Ca2.5Cu3</sub> -S	2.5	3	64	0.22	7.6

**Table 2**Peak areas of different basic sites in CO<sub>2</sub>-TPD.

Catalyst	Basicity site						
	weak	medium	strongly	Medium and strongly	Total		
Cat <sub>Cu3</sub>	0.060	0.065	0.063	0.128	0.187		
Cat <sub>Ca2.5</sub>	0.117	0.197	0.181	0.378	0.495		
Cat <sub>Ca1Cu3</sub>	0.075	0.078	0.068	0.146	0.221		
Cat <sub>Ca1.5Cu3</sub>	0.067	0.104	0.079	0.183	0.250		
Cat <sub>Ca2Cu3</sub>	0.068	0.100	0.094	0.195	0.262		
Cat <sub>Ca2.5Cu3</sub>	0.080	0.107	0.180	0.286	0.366		
Cat <sub>Ca3Cu3</sub>	0.071	0.111	0.110	0.221	0.292		

EDX image shows that Cu and Ca are highly and uniformly dispersed throughout the catalyst.

To verify the influence of supported metal on the crystalline structure of samples, XRD patterns were measured (Fig. 2a). The result showed that all samples presented a crystal phase of  $\gamma\text{-}Al_2O_3$ , and no peaks belonging to Cu oxides and Ca-compounds were discovered, indicating the high dispersion of metals.

To further investigate the active composition of  $Cat_{CaxCu3}$ , XPS analysis was implemented (Fig. 2). The spin-orbit splitting separation  $\delta$  (Ca  $2p_{3/2}$  – Ca  $2p_{1/2}$ ) of Ca-compound is  $3.5\pm0.2$  eV [40]. As shown in Fig. 2b, the Ca 2p of  $Cat_{Ca2.5}$  was deconvolved into four different characteristic peaks, whereas in  $Cat_{Ca2.5Cu3}$ , there are only two deconvoluted distinct peaks. Among them, the characteristic peaks at ca. 346.4 eV and ca.359.8 eV correspond to  $2p_{3/2}$  and  $2p_{1/2}$  peak of CaO respectively [40,

41], while the characteristic peak at ca. 348 eV and ca.351.5 eV were corresponding to  $2p_{3/2}$  and  $2p_{1/2}$  characteristic peak of CaCO $_3$  or Ca (NO $_3$ ) $_2$  which was not completely pyrolyzed [40]. To further verify the presence of Ca-compounds, the C 1 s diffraction patterns Cat<sub>Ca2.5</sub> and Cat<sub>Cu3</sub> were compared (Fig. 2c), and it can be observed that no other characteristic peak was present except for the C-C peak (284.8 eV) and C=O peak (289 eV) caused by carbon pollution [42]. As a result, the characteristic peak of the Ca 2p diffraction pattern at ca. 348 eV was not corresponding to CaCO $_3$  [43,44]. To further demonstrate the existence form of Ca, thermogravimetric (TG) and differential thermogravimetric (DTG) analyses were performed on Ca(NO $_3$ ) $_2$ ·4 H $_2$ O within the calcination range of 30–800 °C.

As shown in Fig. 2g, the weight loss of the Ca(NO<sub>3</sub>)<sub>2</sub>·4 H<sub>2</sub>O in the N<sub>2</sub> atmosphere started at 30 °C, a slow mass loss of 4.6% occurred between 30 °C and 129.45 °C, followed by a rapid mass loss of 24.81% until 235.8 °C. According to the DTG results, Ca(NO<sub>3</sub>)<sub>2</sub>·4 H<sub>2</sub>O experienced three weight loss stages below 800 °C: The first stage involves the removal of adsorbed water and crystalline water. In contrast, the second stage involves the removal of crystalline water, and the third stage involves the release of O<sub>2</sub> and NO. The total weight loss below 500 °C is 29.41%, which is similar to the weight loss of Ca(NO<sub>3</sub>)<sub>2</sub>·4 H<sub>2</sub>O when completely dehydrated into Ca(NO<sub>3</sub>)<sub>2</sub>. Although Ca(NO<sub>3</sub>)<sub>2</sub> may undergo further decomposition at 490 °C, the presence of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> promotes this process, while the presence of Cu<sub>x</sub>O slows it down [45]. Based on XPS results, the surface of Cat<sub>Ca2.5</sub> contains both Ca(NO<sub>3</sub>)<sub>2</sub> and CaO, whereas the surface of Cat<sub>Ca2.5</sub>Cu<sub>3</sub> only contains Ca(NO<sub>3</sub>)<sub>2</sub>.

The O 1 s peaks of Cat<sub>CaxCuv</sub> samples were further analyzed in Fig. 2d, the peaks located at ca. 530.1 eV (O-I), ca. 531 eV (O-II), ca. 532 eV (O-III) and ca. 532.8 eV (O-IV) are assigned to the lattice oxygen in CuO [46] or/and CaO [47], chemisorbed oxygen, lattice oxygen in Al<sub>2</sub>O<sub>3</sub> [48], and hydroxyl oxygen and/or surface adsorbed oxygen. In the Cat<sub>CaxCuv</sub> samples, the O-III content corresponds to the VOs concentration [48-50]. The O-IV of Cat<sub>Cu3</sub> was attributed to the oxygen species that are weakly bound (such as H<sub>2</sub>O or O<sub>2</sub> adsorbed onto the catalyst's surface) and/or -OH groups, for  $\text{Cat}_{\text{Ca2.5Cu3}}$  and  $\text{Cat}_{\text{Ca2.5}},$  the O-IV might also be related to O in  $NO_3$ . The surface of the  $Cat_{Ca2.5}$  catalyst showed the presence of only three oxygen species, but no O-II was detected, suggesting that there were no VOs on the surface of Cat<sub>Ca2.5</sub>. The percentage of O-II for Cat<sub>Cu3</sub> and Cat<sub>Ca2.5Cu3</sub> are 31.89% and 40.9%, respectively. The higher proportion of VOs in Cat<sub>Ca2.5Cu3</sub> indicates stronger surface reactivity, leading to improved interactions with H2S during the removal process [51].

Fig. 2e shows the characteristic peaks of Cu  $2p_{3/2}$  of  $Cat_{Cu3}$  and  $Cat_{Ca2.5Cu3}$ , deconvoluted into two peaks. The binding energy characteristic peak at ca. 934.7 eV implies the existence of Cu(II), and the peak

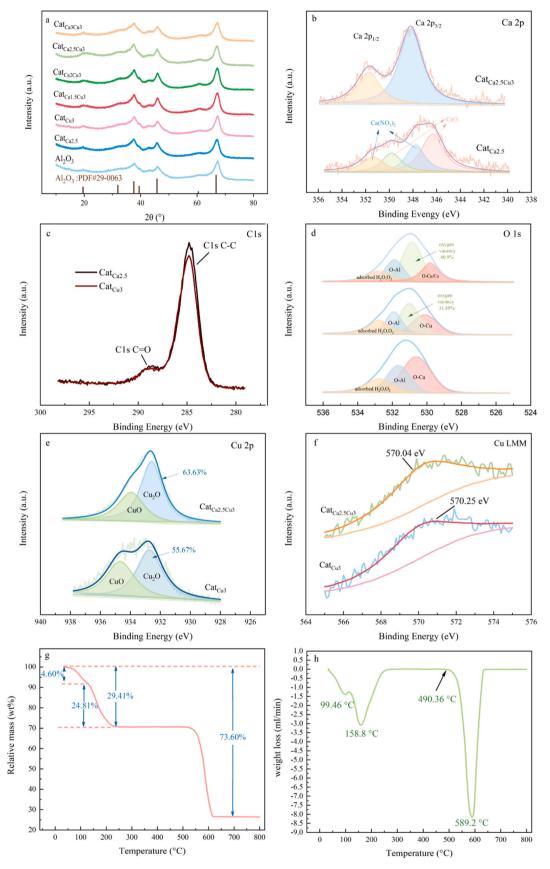


Fig. 2. XRD (a), XPS of Ca 2p (b), C 1 s (c), O 1 s (d), Cu 2p (e), and CuLMM (f) pattern of Cat<sub>CaxCu3</sub>, and TG (g) and DTG (h) of Cat<sub>Ca2.5Cu3</sub>.

at ca. 932.8 eV corresponds to the Cu(0)/Cu(I) [52,53]. To identify the existence of Cu(0) and Cu(I), Cu LMM peaks can be used to distinguish these copper species. As shown in Fig. 2f, the Cu LMM peaks of  $Cat_{Cu3}$  and  $Cat_{Ca2.5Cu3}$  occurred at ca. 570 eV, indicating the existence of Cu(I) [54,55]. The change of binding energy of Cu 2p and Cu LMM after introducing Ca-compounds suggests the presence of a chemical bonding interface between Cu oxides and Ca-compounds rather than just physical contact between two separate phases [56]. Moreover, the introduction of  $Ca(NO_3)_2$  increases the proportion of Cu(I) peak area (from 55.67% to 63.63%), which may be attributed to the doping of  $Ca(NO_3)_2 \cdot 4$  H<sub>2</sub>O. As a result, some of the Cu(II) species gain electrons and transform into Cu (I) [57,58]. The formation of partial VOs is achieved by eliminating some O atoms from the CuO [59].

To investigate the fine structure of  $Cat_{Ca2.5Cu3}$  nano-sheets further, the TEM images and crystal size distribution (Fig. 3) were also analyzed. As a comparison, TEM of  $Al_2O_3$  is also provided in Fig. S7. Plentiful nanoparticles and their crisscross needle-like structures can be observed in the TEM image of  $Cat_{Ca2.5Cu3}$  (Fig. 3a). Form Fig. S7, the overall thickness of  $Al_2O_3$  is greater than  $Cat_{Ca2.5Cu3}$ , with  $Al_2O_3$  featuring overlapping edge sheets, while the edges of  $Cat_{Ca2.5Cu3}$  are evidently extended into thin nanosheets. This result is consistent with the SEM results, confirming the formation of nanosheets on the surface of  $Cat_{Ca2.5Cu3}$ . Also, numerous uniformly distributed pores with sizes less than 1 nm on the nanosheets (indicated by the red circles in Fig. 3c). The enlarged HRTEM image (Fig. 3c) shows obvious lattice fringes, the

lattice fringes of 0.232, 0.216, 0.150 and 0.257 nm were attributed to the (111) lattice plane of CuO, the (006) lattice plane of  $Al_2O_3$ , the (220) lattice plane of  $Cu_2O$ , and the (001) lattice plane of  $Ca(NO_3)_2$ , respectively. Furthermore, the HRTEM images were subjected to fast Fourier transform (FFT) and inverse FFT analysis (Fig. S8). The results indicated that the nanosheets were formed by the staggered combination of metals with different crystal structures. Still, the composition of each part was different, which indicated that CuO,  $Cu_2O$ , and  $Ca(NO_3)_2$  coexisted in the nanosheets, whereas the distribution was random. In addition, Fig. 3b showcases a selected area electron diffraction (SAED) image of a portion of the nanosheet. This image indicated that the  $Cat_{Ca2.5Cu3}$  exhibited polycrystalline characteristics, and the concentric diffraction ring pattern can be assigned to the CuO (111),  $Al_2O_3$  (006),  $Cu_2O$  (220), and  $Ca(NO_3)_2$  (001), respectively.

To further verify the existence of VOs, EPR measurements were performed. For Cu-based catalysts, the EPR spectrum (Fig. 4a) shows visible EPR signals, and after adding the Ca compounds, the vacancy signal increased. The  $Cat_{Ca2.5Cu3}$  exhibited the highest EPR signal, and the signal at 60 °C was higher than that at 25 °C (Fig. 4b), which showed that slight heating was beneficial to the activation of more VOs. In contrast, there was no appreciable signal of Ca/Al $_2$ O $_3$ , suggesting that no VOs existed in Ca/Al $_2$ O $_3$ , and VOs were primarily formed due to the oxygen deficiency in Cu $_x$ O. The doping of Ca-compounds resulted in the shedding of oxygen from the Cu $_x$ O lattice (the proportion of Cu(I) increased) resulting in the formation of more VOs, which was consistent

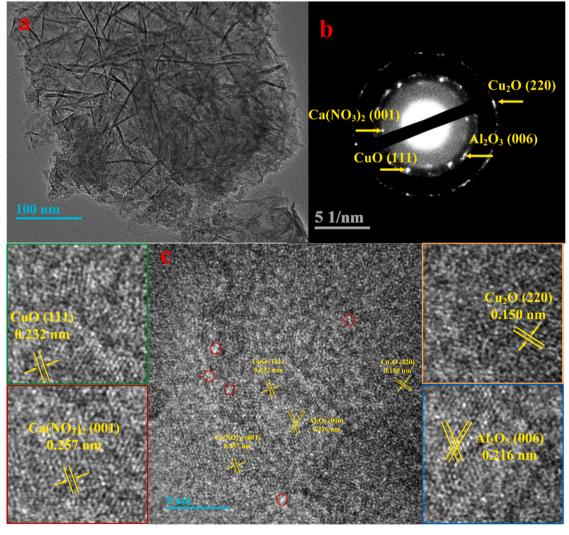
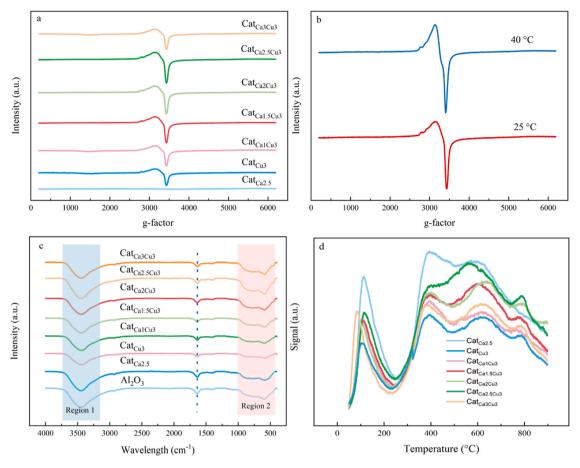


Fig. 3. TEM (a), SAED (b), and HRTEM (c) image of Cat<sub>Ca2.5Cu3</sub> nanosheet.



 $\textbf{Fig. 4.} \ \ \text{EPR-vacancy of all Ca-Cu/Al}_2O_3 \ \ \text{catalysts (a), and Cat}_{\text{Ca2.5Cu3}} \ \ \text{at different temperatures (b), CO}_2\text{-TPD (c)} \ \ \text{and FTIR (d) of all Ca-Cu/Al}_2O_3 \ \ \text{catalysts.}$ 

with the XPS results.

Results from FT-IR measurements were depicted in Fig. 4c, and the spectra of Al<sub>2</sub>O<sub>3</sub> were presented for reference purposes. The peaks attributed to -OH stretching were identified in region 1  $(3300-3600 \text{ cm}^{-1})$ , while the vibrations related to  $M^{2+}$ - $O^{2-}$  were shown in the peaks  $<1000\,\mathrm{cm}^{-1}$  (region 2). The peak at  $1630\,\mathrm{cm}^{-1}$  corresponded to O-CO stretching or H-OH bending vibrations [3,23]. To gain insight into the distribution of basic sites on the catalyst surface, CO<sub>2</sub>-TPD analysis was performed. Basic sites were classified into weak (<300 °C), medium (300-500 °C), and strong (>500 °C) based on CO<sub>2</sub> desorption temperature (Fig. 4d, Fig. S9) [60]. The CO<sub>2</sub> peak below 300 °C represented CO<sub>2</sub> desorption adsorbed on the catalyst surface hydroxyl groups, while the peak at 300–500 °C was related to M<sup>2+</sup>-O<sup>2-</sup> acid-base pairs [60]. According to FTIR results, hydroxyl groups were related to the hydrophilicity of Al<sub>2</sub>O<sub>3</sub> which was beneficial to removing H<sub>2</sub>S. In general, peaks above 500 °C indicated coordination of unsaturated O<sup>2</sup>-, with higher concentrations indicating more VOs on the catalyst. EPR-vacancy results showed no VOs in CatCa2.5, but the CatCa2.5 exhibited the strongest CO<sub>2</sub> desorption peak in the range of 500-700 °C, indicating that this peak was not related to VOs. The Cu-based catalyst showed four CO2 adsorption characteristic peaks. In contrast, the Ca/Al<sub>2</sub>O<sub>3</sub> sample had only three surface basic sites, indicating that the peaks around 800 °C were ascribed to the coordination of unsaturated  ${
m O}^{2}$ . The 500–700 °C peaks may be attributed to the interaction between the highly dispersed Ca(NO<sub>3</sub>)<sub>2</sub>/Cu<sub>x</sub>O and the Al<sub>2</sub>O<sub>3</sub> support [61]. The presence of this complex strong basic site may enhance the desulfurization effect of the Cu-based catalyst. Correlational analysis between sulfur capacity and areas of three different basic sites and total basic site area (Fig. S10) indicated a strong correlation between sulfur capacity and total basic site area ( $R^2 = 0.87$ ), with a higher correlation between sulfur capacity and medium strong basic sites than weak basic sites. These findings suggested that catalyst surface basic sites positively correlate with desulfurization performance, with surface metal basicity and VOs working synergistically to promote desulfurization.

Basic sites generally exhibit the capability to adsorb and concentrate free radicals [62,63]. This implies that the basic sites might adsorb the  $\cdot$ OH produced by the catalysis of VOs in H<sub>2</sub>O. EPR spectroscopy (Fig. 5) was employed to test this hypothesis to investigate the unpaired electron spins in the catalysts, revealing valuable structural information [64].

The results showed that no signal attributed to unpaired electron states was observed in the EPR spectrum of  $Cat_{Ca2.5}$  without VOs, indicating that this catalyst does not possess the ability to generate ·OH. For Cu-based catalysts, the presence of ·OH was observed to be consistent with the trend of VOs but not directly proportional. All Cu-based catalysts exhibited a significant amount of ·OH, indicating that the doping of  $Ca(NO_3)_2$  increased the VOs in the catalysts, provided basic sites, and enabled the enrichment of ·OH. This adsorptive and enrichment effect plays a crucial role in stabilizing free radicals and creates additional opportunities for subsequent catalytic reactions. Moreover, EPR tests were conducted under different time (Fig. 5b) and temperature (Fig. 5c) conditions, revealing that the catalyst acquires ·OH through its catalytic action on the DMPO, with higher temperatures enhancing this process.

#### 3.2. Catalytic performance

Different Cu-based catalysts with varying Ca metal content were subjected to dynamic  $H_2S$  oxidation adsorption experiments (Fig. 6a, b). The results show that the alumina support had no removal performance on  $H_2S$ , while  $Ca/Al_2O_3$  had very little performance, with a breakthrough sulfur capacity of approximately 12.86 mg  $H_2S/g$  catalyst.  $Cu/Al_2O_3$ 

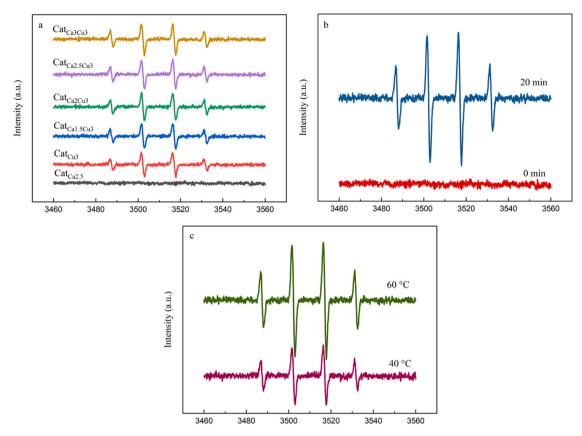


Fig. 5. EPR spectra of  $Cat_{CaxCu3}$  catalysts (a),  $Cat_{Ni2.5Cu3}$  at different time points (b) and different temperature (c).

 $\rm Al_2O_3$  had an ideal catalytic oxidation effect on  $\rm H_2S$ , with a breakthrough sulfur capacity of up to 225.27 mg/g, increasing the breakthrough sulfur capacity with increasing Ca content. The maximum sulfur capacity was observed at a Ca content of 2.5 wt%, reaching 401.34 mg/g.

The catalytic mechanism of the catalyst can be understood by examining its theoretical sulfur capacity (TSC) (Eq. 3). Additionally, The SSA sulfur capacity and the TPV sulfur capacity are also included in the analysis (Table 3).

$$TSC = \frac{m}{M_{metal}} \times M_{H_2S} \times 1000 \tag{3}$$

Where: TSC is the theoretical sulfur capacity of the catalyst (mg H<sub>2</sub>S/g catalyst),  $M_{metal}$  is the atomic mass of a metal substance (g/mol), m is the metal's mass per catalyst (1 g),  $M_{H2S}$  is the molecule mass of H<sub>2</sub>S (34 g/mol)

Al<sub>2</sub>O<sub>3</sub>, Cu<sub>x</sub>O, and Ca-compounds among the prepared catalysts exhibited significantly low H2S desulfurization capacity. However, both Cu<sub>x</sub>O and Ca-compounds demonstrated the highest surface activity, suggesting that the primary active components were CuxO and Ca  $(NO_3)_2$ . The sulfur capacity of  $Cat_{Ca2.5}$  was lower than the TSC, indicating that Ca/Al<sub>2</sub>O<sub>3</sub> only underwent chemical adsorption and lacked catalytic oxidation of H2S. The sulfur capacities of all Cu-based catalysts were higher than the TSC, indicating that there was also catalytic oxidation of H<sub>2</sub>S in addition to chemical adsorption. While individual Ca-compounds did not exhibit catalytic oxidation performance on H<sub>2</sub>S, adding it to Cu/Al<sub>2</sub>O<sub>3</sub> can promote the catalytic activity of Cu-based catalysts. Furthermore, although CatCa2.5Cu3 had the highest sulfur capacity, the SASC and TVSC were lower than those of other Cu-based catalysts. This indicated that for Cat<sub>CaxCu3</sub>, the SSA and pore volume are not the limiting factors for desulfurization. The larger SSA increased the exposure of active sites, thus enhancing the catalyst's performance. However, during the reaction, the generation of desulfurization byproducts led to the collapse of the catalyst's surface nano-sheet structure, gradually diminishing the catalytic reaction. Consequently, the full utilization of the SSA and pore volume could not be achieved.

To evaluate the influence of H<sub>2</sub>O on the removal of H<sub>2</sub>S, dynamic H<sub>2</sub>S removal experiments were performed at different levels of humidity (Fig. 6e, f) and the figure depicting the state of the samples before and after the reaction under different humidity conditions was presented in Fig. S11 and Fig. S12. The results demonstrated the significant influence of H<sub>2</sub>O on the catalytic removal of H<sub>2</sub>S. In the absence of H<sub>2</sub>O, the breakthrough sulfur capacity of H<sub>2</sub>S was only 33.6 mg/g, which is below the TSC. However, under RH 40% and 60%, the catalyst surpassed the TSC by a considerable margin, implying that the catalytic reaction can only persist in the presence of H<sub>2</sub>O. Moreover, investigators observed that water vapor also enhances the elimination of H<sub>2</sub>S by facilitating the dissociation of captured H2S. Additionally, at a relative humidity of 80%, excessive moisture caused catalyst agglomeration (Fig. S12c), preventing H<sub>2</sub>S from reaching the catalyst's active sites and impeding the reaction. Hence, maintaining a suitable level of H2O content is critical to ensure effective catalytic oxidative removal of H2S.

Dynamic removal experiments of  $H_2S$  with  $Cat_{Ca2.5Cu3}$  were conducted at various room temperatures (Fig. 6e, f), and the results indicated that the temperature had a certain impact on  $H_2S$  elimination. The desulfurization performance of the catalyst was enhanced within 40–60 °C, whereas further increasing the temperature led to a decrease. This may be attributed to the positive role that an appropriate temperature played in promoting the diffusion of  $H_2S$  to the surface of the catalyst, fostering the catalytic reaction. In contrast, excessively high temperatures hindered the physical adsorption of  $H_2S$  and  $H_2O$  on the surface of the catalyst.

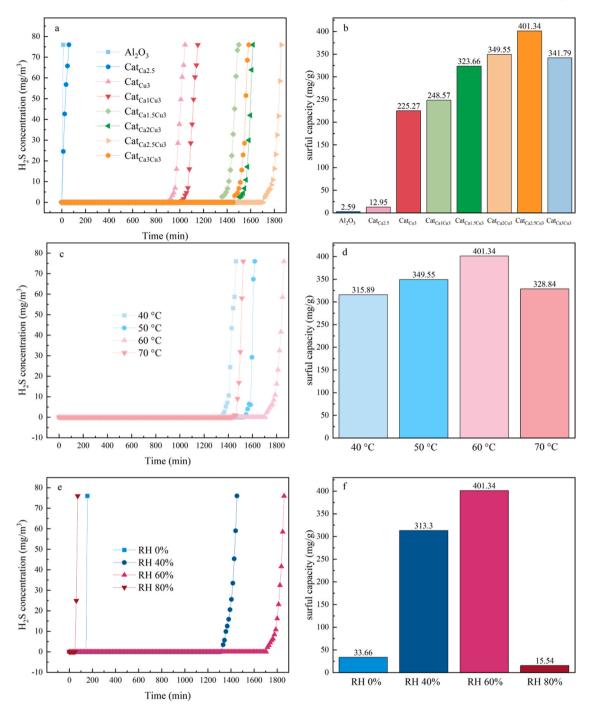


Fig. 6. Breakthrough curves and breakthrough sulfur capacity for catalytic oxidation of  $H_2S$  of  $Cat_{Cax_{Cu3}}$  at 60 °C and relative humidity 60% (a, b) and breakthrough curves and breakthrough sulfur capacity of  $Cat_{Ca2_{.5}Cu3}$  at different humidities (c, d) and relative temperatures (e, f).

#### 3.3. Mechanisms of Cat<sub>Ca2.5Cu3</sub> desulfurization

#### 3.3.1. Analysis of spent catalysts

Fig. S13 displays the  $N_2$  adsorption—desorption and SEM results of the  $Cat_{Ca2.5Cu3}$  catalyst before and after  $H_2S$  desulfurization. The overall structure of the catalyst remained unaffected by the desulfurization process, which still maintained the mesoporous structure with  $H_3$ -type hysteresis loop (Fig. S13a). However, the hysteresis loop weakened. According to the pore size distribution, the reactive adsorption of  $H_2S$  resulted in a reduction of the pore capacity of the catalyst (Fig. S13b, Table 1), indicating that desulfurization products were stored in the pore structure. The SEM results (Fig. S13d) showed that the agglomerates

generated during catalyst desulfurization covered the surface and the layered structure and nanosheets disappeared. According to EDS results (Fig. S13e), elemental sulfur and sulfur compounds covered the catalyst's surface while Cu and Ca compounds were hardly detectable.

To identify the  $\rm H_2S$  desulfurization product on the catalyst, we conducted XRD and XPS analyses on the spent catalysts. XRD pattern of  $\rm Cat_{Ca2.5Cu3}$ -S (Fig. 7a) proved that the  $\rm H_2S$  desulfurization product adsorbed in the deep pore structure was mainly sulfur (PDF#99–0066), and no sulfate or sulfide with Ca or Cu were detected, which may be related to the content lower than the XRD detection limit or high degree of metal dispersion.

The XPS analysis was conducted to further identify the

**Table 3**Theoretical sulfur capacity and actual sulfur capacity of samples.

Samples	TSC (mg/g)	Sulfur capacity			
		mg/g	mg/m <sup>2</sup>	mg/m <sup>3</sup>	
$Al_2O_3$	/	2.59	0.01	5.76	
CaO/Ca(NO <sub>3</sub> ) <sub>2</sub>	Ca. 300	10.9	0.61	363.33	
Cu <sub>x</sub> O	531.2	18	1.20	450.00	
Cat <sub>Ca2.5</sub>	21.25	12.95	0.05	28.78	
Cat <sub>Cu3</sub>	16.5	225.27	1.10	500.60	
Cat <sub>Ca1Cu3</sub>	24.43	248.57	1.27	552.38	
Cat <sub>Ca1.5Cu3</sub>	28.68	323.66	1.69	719.24	
Cat <sub>Ca2Cu3</sub>	32.93	349.55	1.77	794.43	
Cat <sub>Ca2.5Cu3</sub>	37.18	401.34	1.64	716.68	
Cat <sub>Ca3Cu3</sub>	41.43	341.79	1.77	776.80	

desulfurization product on the surface of the catalysts. Fig. 7b shows the S 2p region of the three samples, in this region, the spectrum of  $Cat_{Cu3}$  and  $Cat_{Ca2.5Cu3}$  was deconvolved into 6 peaks. The BEs of S  $2p_{3/2}$  and S  $2p_{1/2}$  appeared at ca. 161.7 eV and 162.8 eV, respectively, suggesting the presence of S in  $S^2$ · [65–67]. The BEs at ca. 163.7 eV and ca.164.7 eV corresponded to the  $2p_{3/2}$  and S  $2p_{1/2}$  of elemental S. Moreover, the peaks appear at ca. 168.6 eV and ca.169.8 eV correspond to the  $2p_{3/2}$  and  $2p_{1/2}$  characteristic peak of  $SO_4^{2^-}$  [68], indicating the further oxidation of elemental S. It was worth noting that  $Cat_{Ca2.5Cu3}$  has 0.1 eV shift compared with  $Cat_{Cu3}$ , which may be due to the existence of S compounds related to Ca. For  $Cat_{Ca2.5}$ , although a weak S 2p characteristic peak could be detected, it could not be deconvolved clearly, and thus the desulfurization product will be judged by Ca 2p. The surface total sulfur content detected by XPS in  $Cat_{Ca2.5}$ ,  $Cat_{Cu3}$ , and  $Cat_{Ca2.5Cu3}$ 

was 2.44%, 16.19%, and 23.89%, respectively. The sulfate detected on the surface was the dominant product for  $\text{Cat}_{\text{Cu}3}$  and  $\text{Cat}_{\text{Ca}2.5\text{Cu}3}$ , accounting for 59.85% and 64.8% respectively, indicating that the doping of  $\text{Ca}(\text{NO}_3)_2$  not only increased the desulfurization performance, but also promoted the conversion of desulfurization products to sulfate.

The Cu  $2p_{3/2}$  peaks of  $Cat_{Cu3}$  and  $Cat_{Ca2.5Cu3}$  (Fig. 7c) were deconvoluted into three distinct peaks at ca. 934.9 eV, ca. 933.3 eV, and ca. 932.2 eV, corresponding to the presence of  $CuSO_4$ ,  $Cu_2S$ , and CuS, respectively [69–72]. Furthermore, the Ca 2p peaks of  $Cat_{Ca2.5}$  (Fig. 7d) can be deconvoluted into 4 distinct characteristic peaks. Among them, the characteristic peaks at ca. 346.5 eV and ca.350.1 eV correspond to  $2p_{3/2}$  and  $2p_{1/2}$  of CaS respectively [73], while the characteristic peak at ca. 347.8 eV and ca.351.4 eV were corresponding to  $2p_{3/2}$  and  $2p_{1/2}$  characteristic peak of  $CaSO_4$  [74]. It is worth noting that the  $Cat_{Ca2.5Cu3}$  only exhibits characteristic peaks corresponding to  $CaSO_4$ , and combined with the S  $CaSO_4$  is can be concluded that the doping of  $CaSO_3$  promotes the oxidation of S.

The detected sulfur content of the  $Cat_{Ca2.5}$  was 2.44%, which is almost identical to the loaded Ca content. This suggested that the desulfurization process of  $Cat_{Ca2.5}$  did not generate elemental sulfur. As a result, according to XPS analysis, when only loaded with Ca, the desulfurization products of the catalyst consist of sulfides and sulfates. However, for  $Cat_{Cu3}$  and  $Cat_{Ca2.5Cu3}$ , the desulfurization process yields sulfides, sulfates, and sulfur. In conclusion, the desulfurization products of  $Cat_{Ca2.5Cu3}$  include  $CaSO_4$ ,  $CuSO_4$ ,  $CuSO_4$ , and S.

#### 3.3.2. DFT calculations

The dynamic H<sub>2</sub>S removal experimental results demonstrate the crucial role of H<sub>2</sub>O in the catalytic removal of H<sub>2</sub>S. However, Ca/Al<sub>2</sub>O<sub>3</sub>

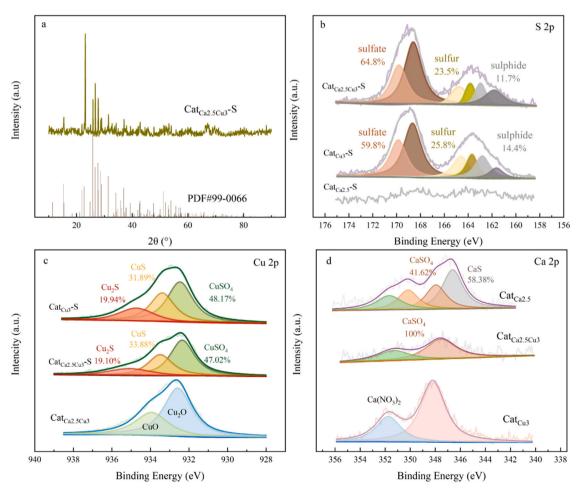


Fig. 7. The XRD (a) and XPS, S 2p (b), Cu 2p (c), and Ca 2p (d) image of Cat<sub>CaxCu3</sub>.

catalysts without VO did not exhibit catalytic  $H_2S$  activity, whereas Cubased catalysts with VOs exhibited efficient desulfurization. This indicates that Cu-based catalysts achieve catalytic oxidation of  $H_2S$  at low temperatures by leveraging the catalytic action of VOs species on  $H_2O$ . DFT calculations were used to investigate the impact of  $Ca(NO_3)_2$ -doping on the formation of VOs. The formation energy of VOs (Ev) was determined using the formula:  $E_V = E_{tot(def)} - E_{tot(no\ def)} + \frac{1}{2}E_{O_2}$ . Here,  $E_{tot}$  (def) and  $E_{tot(no\ def)}$  represent the energy of defective systems or perfect surface,  $E_{O_2}$  means the energy of an  $O_2$  molecule. The formation energies of VOs for these two structures were calculated to be  $-0.75\ eV$  and  $-1.336\ eV$ , respectively. These results indicate that the formation of VOs in both catalysts is spontaneous, and the presence of  $Ca(NO_3)_2$  facilitates the formation of VOs. This observation aligns with the trend observed in the EPR-defect results.

The reaction pathway of critical steps was calculated using the transition state (TS) theory. Fig. 8a, b presented the calculations of the adsorption of  $\rm H_2O$  and its catalytic behavior on the VOs. The computational results showed that for the  $\rm Cu_xO/Al_2O_3$  catalyst, the adsorption of  $\rm H_2O$  and its catalytic conversion to OH at the  $\rm Cu_2O$  site is spontaneous (-0.37 eV) (Fig. 8a). The VOs in  $\rm Cu_2O$  catalyze the hydroxylation of  $\rm H_2O$  (Eq. 4) without undergoing chemical reaction (Eq. 5). And it becomes even more favorable with the doping of  $\rm Ca(NO_3)_2$  (-1.21 eV). Although the hydroxylation of  $\rm H_2O$  at the  $\rm CuO$  site is also spontaneous (Fig. 8b), the formation of the transition state ( $\rm Cu(OH)_2$ ) requires some energy. However, this reaction becomes more favorable after doping  $\rm Ca(NO_3)_2$ . Combining experimental and characterization results, it can be concluded that the basis for the  $\rm H_2S$ -catalyzed oxidation is the hydroxylation of  $\rm H_2O$  by VOs.

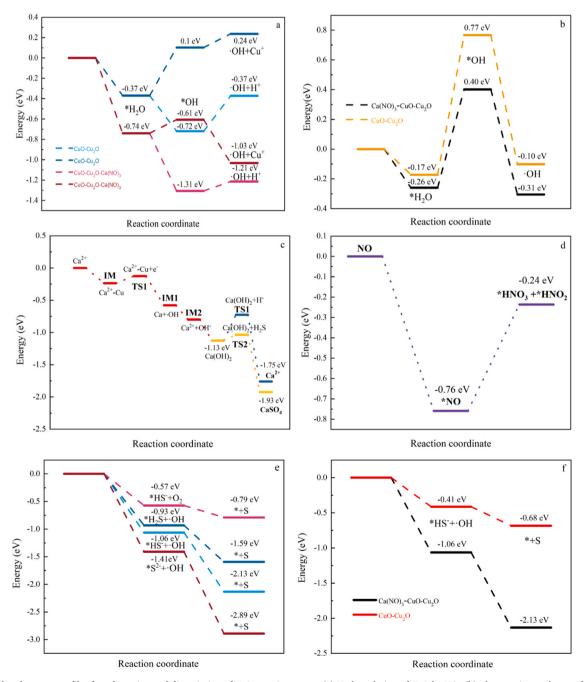


Fig. 8. Calculated energy profiles for adsorption and dissociation of  $H_2S$  over  $Cat_{Ca2.5Cu3}$  (a) Hydroxylation of  $H_2O$  by VOs (b), the reaction pathway of  $Ca^{2+}$  (c), NO cycle (d),  $H_2S/HS$ - oxidation by  $O_2/OH$  (e) over  $Cat_{Ca2.5Cu3}$ , and HS- oxidation by OH of  $Ca(NO_3)_2$ - $Cu_2O$ -CuO and  $Cu_2O$ -CuO (f).

$$Cu_2O + H_2O \xrightarrow{VOs} Cu_2O + \cdot OH + H^+ + e^-$$
 (4)

$$H_2O + Cu_2O \rightarrow 2Cu(OH) \xrightarrow{VOs} 2 \cdot OH + 2Cu^+ + 2e^-$$
 (5)

Furthermore, CO<sub>2</sub>-TPD results showed that the desulfurization performance of  $Cat_{CaxCu3}$  was related to the concentration of VOs and the metal sites.  $Cu/Al_2O_3$  catalyst significantly improved the  $H_2S$  desulfurization performance with the assistance of  $Ca(NO_3)_2$ , suggesting a synergistic catalytic effect between  $Cu_xO$  and  $Ca(NO_3)_2$  that is connected with  $Ca(NO_3)_2$ . In the process of  $H_2S$  desulfurization, a large number of  $H^+$  are generated due to the dissociation of  $H_2S$ , which reduces the pH of the reaction system, and thus lowers the  $H_2S$  removal efficiency [75,76]. Additionally, free radicals are unstable and easily disrupted, leading to their conversion into oxygen and water, which cannot be effectively utilized. Therefore, we hypothesize that  $Ca^{2+}$  (basic site) acts as an intermediate to enrich  $\cdot OH$  and  $H^+$  ions. In this process, the basic site with some free radicals, delaying the  $\cdot OH$  quenching and slowing down the pH decrease, thereby decelerating the catalyst deactivation.

Additionally, the calculations also examined the reaction pathway of  $\text{Ca}^{2+}$  (Fig. 8c). The results showed that the  $\text{Ca}^{2+}$  generated by the dissociation of  $\text{Ca}(\text{NO}_3)_2$  in the water film is initially spontaneously adsorbed on the surface of Cu (intermediate (IM), Fig. S14), then desorbs after adsorbing two e (TS1), and reacts with  $\cdot$ OH (IM1, (Fig. S15)) after electron exchange (IM2) to produce  $\text{Ca}(\text{OH})_2$  (Fig. S16). The heat energy of this reaction is -1.13 eV, respectively, indicating that the response is favorable thermodynamically.  $\text{Ca}(\text{OH})_2$  reacts with  $\text{H}^+$  present in the reaction system to produce  $\text{Ca}^{2+}$  (adsorption energy was -0.62 eV, Fig. 9).

The generated  $\text{Ca}^{2+}$  continues to participate in the cycle, facilitating the dissociation of  $\text{H}_2\text{S}$  and improving the utilization efficiency of  $\cdot\text{OH}$ . Furthermore, the calculation results show that the reaction between Ca (OH) $_2$  and  $\text{H}_2\text{S}$  to form  $\text{CaSO}_4$  is also a spontaneous process (-0.8 eV), which would lead to the direct inactivation of Ca. This result is inconsistent with the experimental results, indicating that  $\text{H}_2\text{S}$  is initially captured and dissociated by the water film rather than directly contacting the active sites.

Furthermore, the  $NO_3$  can combine with  $H^+$  to produce strong oxidizing HNO $_3$  (Fig. S17) [77], which can oxidize HS $^-$ /S $_2$  to form S and generate NO. Based on the experimental results, we hypothesize that this reaction is a cyclic process. Therefore, we calculated the probability of NO being captured by the water film in the presence of VOs. The calculation results show that the adsorption energy of NO being at VOs is -0.76 eV (Fig. 8d). The further reaction with  $H_2O$  to form HNO $_3$  and HNO $_2$  has the energy barrier and the heat of 0.52 eV and -0.24 eV, respectively. This confirms our hypothesis. During this process, the majority of HNO $_2$  is oxidized by oxygen to form HNO $_3$ , while a small portion of oxidized  $H_2S$  forms S and generates  $N_2$ , which escapes and no longer participates in the cyclical reaction. This continues until all the N is converted to  $N_2$  and escapes, at which point the reaction stops.

In addition to being hydroxylated by VO species, H<sub>2</sub>O also serves the role of capturing and dissociating H<sub>2</sub>S into H<sup>+</sup>, HS<sup>-</sup>, and S<sup>2-</sup>. The reaction

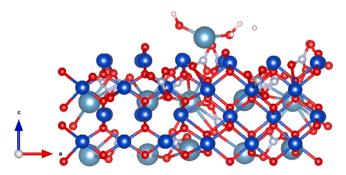


Fig. 9. Adsorption configuration diagram of Ca(OH)<sub>2</sub> adsorb H<sup>+</sup>.

pathways of HS<sup>-</sup> and S<sup>2-</sup> were further calculated (Fig. 8e, f). The results indicate that  $\cdot$ OH oxidizes HS<sup>-</sup> into adsorbed S more readily than O<sub>2</sub>, and HS<sup>-</sup>/S<sup>2-</sup> is more easily oxidized than H<sub>2</sub>S (Fig. 8e). The generated S will desorb from the active site and migrate into the pores of the catalyst (Fig. S18). The adsorption energy of HS<sup>-</sup> oxidized was reduced from -0.68 eV to -2.13 eV with the doping of Ca (Fig. 8f), indicating that adding Ca increases the catalytic oxidation efficiency of H<sub>2</sub>S.

#### 3.3.3. Desulfurization mechanisms

Based on the characterization analysis, experimental and DFT calculation results mentioned above, a rational reaction mechanism for  $\rm H_2S$  desulfurization on  $\rm Cat_{Ca2.5Cu3}$  in low temperature is proposed (Fig. 10).

First, a portion of  $H_2O$  in the gas mixture adsorbs on the catalyst surface through hydrogen bonding, forming a layer of water film. After being captured by the water film,  $H_2S$  dissolves and dissociates into  $H^+$  and  $HS^-$  (Eqs. 6–8). Another portion of  $H_2O$  adsorb on  $Cu_xO$  (active sites) (Eqs. 9–10), which are catalytically oxidized by VOs to form  $\cdot OH$  (Eqs. 11–12). Subsequently, a fraction of these radicals catalytically oxidizes  $HS^-$  and  $S^{2-}$  into S (Eqs. 13–14). Furthermore,  $S^{2-}$  and  $HS^-$  can also be directly oxidized to S by the adsorbed  $O_2$  (Eqs. 15–16). This underlying mechanism allows  $Cat_{CH}$ 3 to catalyze the oxidation of  $H_2S$ .

$$H_2S(g) \rightarrow H_2S(ads)$$
 (6)

$$H_2S(ads) \xrightarrow{water film} H^+ + HS^-$$
 (7)

$$HS^- \xrightarrow{\text{water film}} H^+ + S^{2-}$$
 (8)

$$H_2O + Cu_2O \rightarrow Cu^1OCu^2 - O_{w + H_L}^{H_a}$$
 (9)

$$H_2O + CuO \rightarrow Cu(OH)_2 \tag{10}$$

$$Cu(OH)_2 \longrightarrow^{VOs} Cu^{2+} + 2 \cdot OH + 2e^-$$
 (11)

$$2Cu^{1}OCu^{2} - O_{w \cdot H_{a}}^{H_{a}} \rightarrow Cu_{2}O + O_{w}H_{b} + H_{a}^{+} + e^{-}$$
(12)

$$HS^- + \cdot OH \rightarrow H_2O + S\downarrow + e^-$$
 (13)

$$S^{2-} + \cdot OH + H^+ \rightarrow H_2O + S\downarrow + e^-$$
 (14)

$$4HS^{-} + *O_2 \rightarrow 2H_2O + 4S\downarrow \tag{15}$$

$$2S^{2-} + *O_2 + 4H^+ \rightarrow 2H_2O + 2S\downarrow \tag{16}$$

Although Ca/Al $_2$ O $_3$  cannot directly utilize  $H_2$ O at low temperatures, the primary sites provided by  $Ca^{2+}$  (obtained by Eq. 17) can accumulate the electrons generated in the above reaction, forming a high-density electron cloud (Eq. 18). This attracts the enrichment of  $\cdot$ OH on Ca, forming a stable intermediate Ca(OH) $_2$  (Eq. 19), which then reacts with  $H^+$  in the reaction system (Eq. 20) to promote the dissociation of  $H_2$ S (Eqs. 6–7) and the generation of  $\cdot$ OH (Eq. 11).

 $NO_3$  can react with  $H^+$  to form a strong oxidant,  $HNO_3$ , which directly oxidizes  $HS^-/S^{2-}$  to S (Eqs. 21–22). NO, produced as a reaction product, can be captured by VOs and further reacts with  $H_2O$  to generate  $HNO_3$  and  $HNO_2$  (Eq. 23), which continue to react with  $HS^-/S^{2-}$ . Most of the  $HNO_2$  will be oxidized to  $HNO_3$  by the adsorbed  $O_2$  (Eq. 24).  $N_2$  from  $HNO_2$  and  $HS^-/S^{2-}$  reaction will continuously overflow without further reactions (Eq. 25). This reaction will cycle until all the N overflows. Therefore, the presence of  $Ca(NO_3)_2$  can effectively improve the utilization rate of  $\cdot OH$  and continuously consume  $H_2S$ , thus accelerating the catalytic rate.

$$Ca(NO_3)_2 \longrightarrow^{water film} Ca^{2+} + 2NO_3^-$$
 (17)

$$Ca^{2+} + 2e^{-} \longrightarrow^{basic\ sites} Ca$$
 (18)

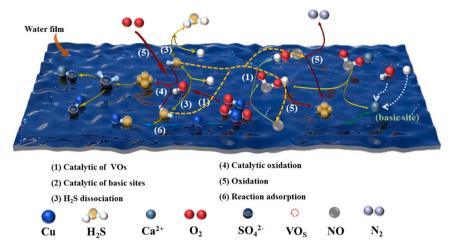


Fig. 10. The proposed desulfurization mechanism of Cat<sub>Ca2.5Cu3</sub>.

$$Ca + \cdot OH \rightarrow Ca(OH)$$
, (19)

$$Ca(OH)_2 + 2H^+ \rightarrow Ca^{2+} + 2H_2O$$
 (20)

$$NO_3^- + H^+ \rightarrow HNO_3 \tag{21}$$

$$HNO_3 + S^{2-} + HS^{-} + 2H^{+} \rightarrow NO + 2H_2O + 2S\downarrow + e^{-}$$
 (22)

$$2NO + H_2O \longrightarrow^{VOs} HNO_3 + HNO_2$$
 (23)

$$2HNO_2 + O_2 \rightarrow 2HNO_3 \tag{24}$$

$$2HNO_2 + S^{2-} + HS^{-} + 5H^{+} + 2e^{-} \rightarrow 2S\downarrow + N_2\uparrow + 4H_2O$$
 (25)

During the reaction process, S<sup>2-</sup> will react with Cu<sup>2+</sup> to generate CuS.

$$Cu^{2+} + S^{2-} \rightarrow CuS \tag{26}$$

Eventually, the produced S undergoes further oxidation through adsorbed oxygen and concurrently reacts with  $H_2O$  to form  $H_2SO_4$  (Eq. 27). As the  $H_2SO_4$  reacted with CuO and Ca(OH)<sub>2</sub>, sulfate was formed (Eq. 28). Gradually, desulfurization came to a halt due to active centers disappearing, and sulfur and sulfate accumulation.

$$S + 3/2O_2 + H_2O \rightarrow H_2SO_4$$
 (27)

$$H_2SO_4 + CuO + Ca(OH)_2 \rightarrow CuSO_4 + CaSO_4 + 3H_2O$$
 (28)

In summary, the VOs provided by  $Cu_xO$  are essential for the low-temperature removal of  $H_2S$ . The synergistic interaction between VOs and  $Ca(NO_3)_2$  is the fundamental reason behind the excellent catalytic performance of  $Cat_{Ca2.5Cu3}$  at low temperatures.

### 3.4. Sulfur recovery

The generation of sulfur salts and sulfides is approximately equal to the theoretical sulfur capacity, and the production of S is estimated by subtracting the theoretical sulfur capacity from the measured sulfur capacity. Approximately 0.34 g of S was adsorbed in the pores of 1 g Ca $_{2.5\text{Cu}3}$  spent catalyst (Sulfur selectivity > 90%). Sulfur recovery experiments were conducted at temperatures above the sulfur dew point to enhance economic benefits. Approximately 0.31 g of sulfur was obtained as a recovery from 1 g of catalyst (Fig. S19). The resource recovery reduces the cost of  $H_2S$  removal and improves the sulfur yield.

#### 4. Conclusions

In conclusion, a series of Ca-Cu<sub>x</sub>O/Al<sub>2</sub>O<sub>3</sub> were successfully

synthesized by the excessive impregnation method and used for H<sub>2</sub>S removal at a low temperature. Optimize the Ca content, reaction temperature, and humidity by H2S dynamic removal experiments; the experiments results showed that the Ca-Cu<sub>x</sub>O/Al<sub>2</sub>O<sub>3</sub> catalyst with 2.5 wt% Ca has the best H<sub>2</sub>S removal capacity at 60 °C and RH 60%, reaching 401.34 mg H<sub>2</sub>S/g catalyst. H<sub>2</sub>O plays a vital role in the catalytic oxidation of H<sub>2</sub>S: the catalytic oxidation does not occur without H<sub>2</sub>O. The XPS, TG, and TEM characterizations exhibited that the active components of the catalyst were Ca(NO<sub>3</sub>)<sub>2</sub>, Cu<sub>2</sub>O, and CuO, which interlaced to form nanosheets, thereby increasing the contact area with H<sub>2</sub>S. Moreover, the XPS, EPR, FTIR, and CO<sub>2</sub>-TPD characterizations demonstrated that the Ca-Cu<sub>x</sub>O/Al<sub>2</sub>O<sub>3</sub> catalyst possesses abundant VOs and basic sites. The H<sub>2</sub>S removal performance was strongly correlated with the sum of moderate-basicity sites (i.e., VOs) and strong-basicity sites (i.e., metallic sites), which collectively promote the generation of ·OH. In addition, although Ca/Al<sub>2</sub>O<sub>3</sub> has many basic sites, it lacks VOs, resulting in no generation of ·OH and no catalytic effect on H<sub>2</sub>S. This signifies that VOs serve as the foundation for the generation of ·OH, which in turn is the basis for the catalytic oxidation of H<sub>2</sub>S. Furthermore, the XPS characterization of  $Cat_{Ca2.5Cu3}$  exhibited the  $H_2S$  desulfurization products were CaSO<sub>4</sub>, CuSO<sub>4</sub>, CuS, and S. According to the experiment, characterization, and DFT results, a mechanism of H<sub>2</sub>S removal is proposed, which involves physical adsorption, chemical adsorption, and catalytic oxidation. The catalytic oxidation of sulfide anions by ·OH produced via hydroxylation of H<sub>2</sub>O by VOs is not the only mechanism involved. The redundant ·OH adsorbed on the basic sites on the catalyst surface can buffer the pH and promote the dissociation of H2S. In addition, the NO<sub>3</sub> species reacted with H<sup>+</sup> to oxidize the anionic sulfur species. The above cyclic process could alleviate the deactivation of the Ca-Cu/Al<sub>2</sub>O<sub>3</sub> catalyst. Furthermore, we have also found that the catalyst deactivates before fully utilizing the pore volume. Sulfur recovery from the spent catalysts was possible after the reaction. This suggests that there is potential for further modification and design of the catalyst's active sites to achieve higher H2S removal capacity.

#### CRediT authorship contribution statement

Mengxue Yin: Writing – original draft, Validation, Investigation, Formal analysis. Hailong Wang: Validation, Investigation. Wenqing Zhang: Writing – original draft, Formal analysis. Yan Zheng: Writing – review & editing. Long Zhao: Validation. Feiyue Fan: Writing – review & editing, Conceptualization. H. Hou: Writing – review & editing, Resources, Project administration. Suresh C. Pillai: Writing – review & editing. Hongliang Yin: Investigation. Zhihao Wu: Validation.

#### **Declaration of Competing Interest**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### **Data Availability**

No data was used for the research described in the article.

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#### Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at doi:10.1016/j.apcatb.2024.123981.

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